

# MTR08114 Robotics Dynamics

Yasser F. O. Mohammad

# REMINDER 1: The whole Jacobian (METHOD 1)

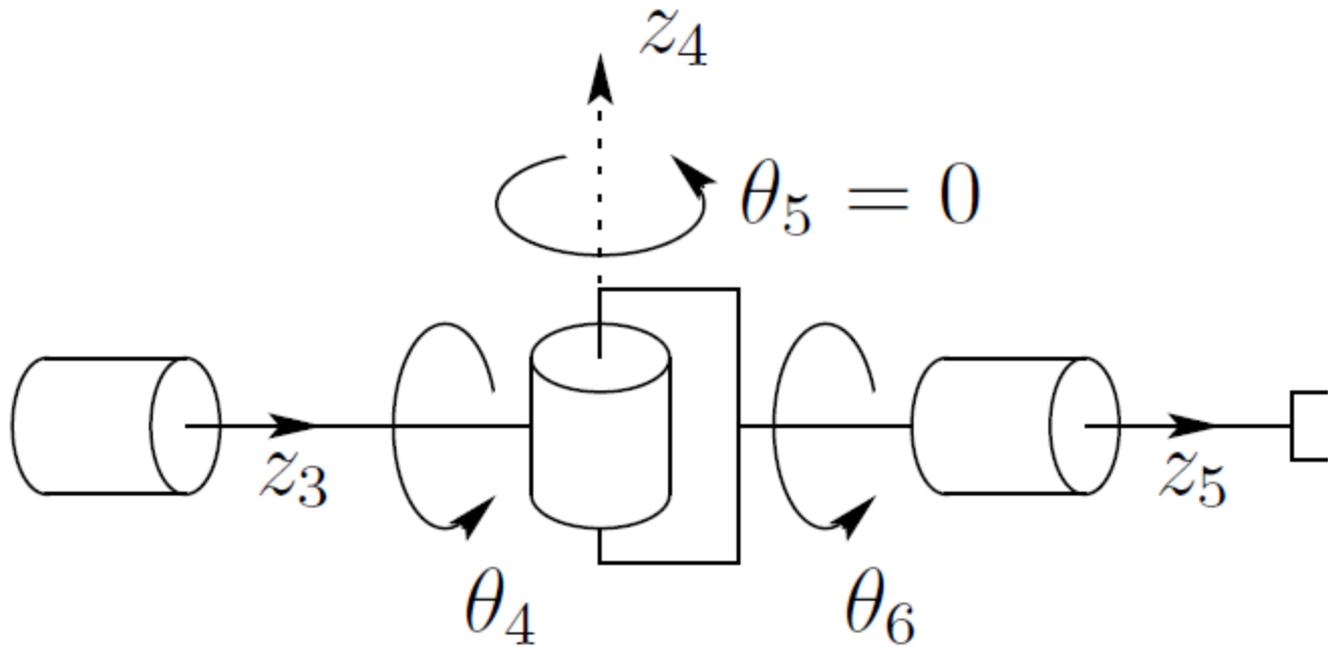
- Revolute Joint

$$J_i = \begin{bmatrix} z_{i-1} \times (o_n - o_{i-1}) \\ z_{i-1} \end{bmatrix}$$

- Prismatic Joint

$$J_i = \begin{bmatrix} z_{i-1} \\ 0 \end{bmatrix}$$

## REMINDER 2: Wrist Singularities

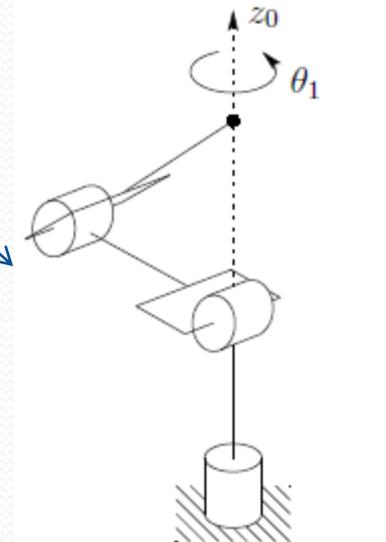
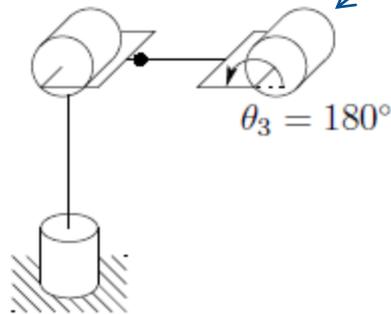
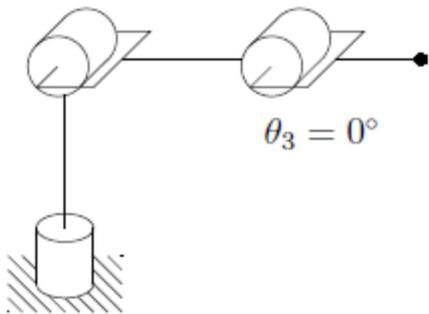


- Whenever  $z_3$  and  $z_5$  are aligned
- Prove it

# REMINDER 3: Elbow Singularity

$$J_{11} = \begin{bmatrix} -a_2 s_1 c_2 - a_3 s_1 c_{23} & -a_2 s_2 c_1 - a_3 s_{23} c_1 & -a_3 c_1 s_{23} \\ a_2 c_1 c_2 + a_3 c_1 c_{23} & -a_2 s_1 s_2 - a_3 s_1 s_{23} & -a_3 s_1 s_{23} \\ 0 & a_2 c_2 + a_3 c_{23} & a_3 c_{23} \end{bmatrix}$$

$$\det J_{11} = a_2 a_3 s_3 (a_2 c_2 + a_3 c_{23}).$$



# REMINDER 4: Resolved Motion Rate Control (Whitney 1972)

$$\delta x = J(\theta)\delta\theta$$

Outside singularities

$$\delta\theta = J^{-1}(\theta)\delta x$$

Arm at Configuration  $\theta$

$$x = f(\theta)$$

$$\delta x = x_d - x$$

$$\delta\theta = J^{-1}\delta x$$

$$\theta^+ = \theta + \delta\theta$$

# REMINDER 5: How to calculate $J^+$

- Most difficult method (from definition):

$$J^+ = \left( J^T J \right)^{-1} J^T$$

- Simplest Method (SVD):

$$J = U \Sigma V^T \quad \sigma_{ij}^+ = 1 / \sigma_{ij}, \quad \text{when } \sigma_{ij} \neq 0$$

$$J^+ = U^T \Sigma^+ V$$

# REMINDER 6: Manipulability

$$\mu = \prod_{i=1}^m \sigma_{ii}$$

If the robot is not redundant ( $n \leq 6$ )

$$\mu = |\det J|$$

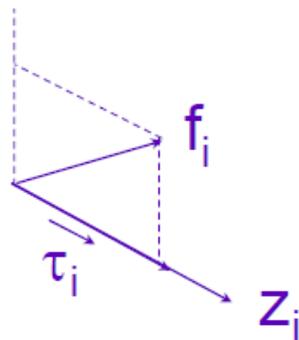
# REMINDER 7: Velocity Force Duality

$$\zeta = J\dot{\theta}$$

$$\tau = J^T F$$

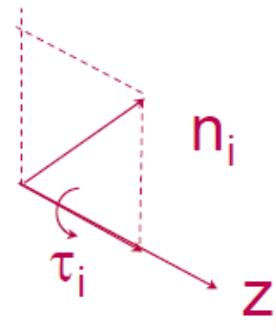
$$F = \begin{bmatrix} f \\ n \end{bmatrix}$$

# REMINDER 8: How to do the elimination



Prismatic Joint

$$\tau_i = f_i^T Z_i$$



Revolute Joint

$$\tau_i = n_i^T Z_i$$

**Algorithm**  ${}^n f_n = {}^n f$

$${}^n n_n = {}^n n + {}^n P_{n+1} \times {}^n f$$

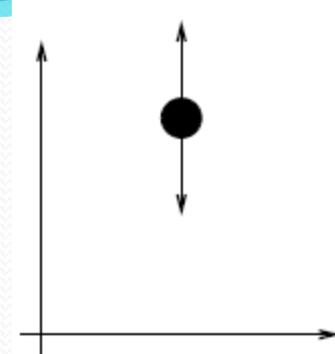
$${}^i f_i = {}^i R_{i+1} \cdot {}^i f_{i+1}$$

$${}^i n_i = {}^i R_{i+1} \cdot {}^i n_{i+1} + {}^i P_{i+1} \times {}^i f_i$$

# What is dynamics

- Relationship between forces and motion
- Two approaches:
  - Traditional Newton laws approach
  - Euler-Lagrange formulation
- In robotics we use Euler-Lagrange formulation because it is MUCH easier for complex objects.

# Motivation (1D system)



$$m\ddot{y} = f - mg$$

$$m\ddot{y} = \frac{d}{dt}(m\dot{y}) = \frac{d}{dt} \frac{\partial}{\partial \dot{y}} \left( \frac{1}{2} m \dot{y}^2 \right) = \frac{d}{dt} \frac{\partial \mathcal{K}}{\partial \dot{y}}$$

$$mg = \frac{\partial}{\partial y}(mgy) = \frac{\partial \mathcal{P}}{\partial y}$$

$$\mathcal{L} = \mathcal{K} - \mathcal{P} = \frac{1}{2} m \dot{y}^2 - mgy$$

$$\frac{\partial \mathcal{L}}{\partial \dot{y}} = \frac{\partial \mathcal{K}}{\partial \dot{y}} \quad \text{and} \quad \frac{\partial \mathcal{L}}{\partial y} = -\frac{\partial \mathcal{P}}{\partial y}$$

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{y}} - \frac{\partial \mathcal{L}}{\partial y} = f$$

# Eular- Lagrange Equation

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{q}_i} - \frac{\partial \mathcal{L}}{\partial q_i} = \tau_i \quad i = 1, \dots, n$$

# Kinetic Energy

$$\mathcal{K} = \frac{1}{2}mv^T v + \frac{1}{2}\omega^T \mathcal{I}\omega$$

Translation

Rotation

Inertia Tensor

# Calculating Inertia Tensor in Fixed Frame

$$I = \begin{bmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{bmatrix}$$

$$I_{xx} = \int \int \int (y^2 + z^2) \rho(x, y, z) dx dy dz$$

$$I_{yy} = \int \int \int (x^2 + z^2) \rho(x, y, z) dx dy dz$$

$$I_{zz} = \int \int \int (x^2 + y^2) \rho(x, y, z) dx dy dz$$

$$I_{xy} = I_{yx} = - \int \int \int xy \rho(x, y, z) dx dy dz$$

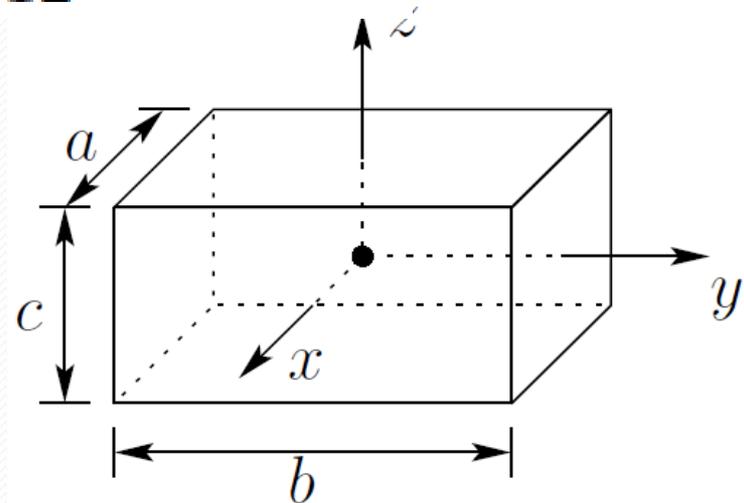
$$I_{xz} = I_{zx} = - \int \int \int xz \rho(x, y, z) dx dy dz$$

$$I_{yz} = I_{zy} = - \int \int \int yz \rho(x, y, z) dx dy dz$$

# Example (Uniform Solid)

$$I_{xx} = \int_{-c/2}^{c/2} \int_{-b/2}^{b/2} \int_{-a/2}^{a/2} (y^2 + z^2) \rho(x, y, z) dx dy dz = \rho \frac{abc}{12} (b^2 + c^2)$$

$$I_{yy} = \rho \frac{abc}{12} (a^2 + c^2) \quad ; \quad I_{zz} = \rho \frac{abc}{12} (a^2 + b^2)$$



# Moving Inertia Tensor Between Frames

$$\mathcal{I} = R I R^T$$

# Kinetic Energy for N Links Robot

$$v_i = J_{v_i}(q)\dot{q}, \quad \omega_i = J_{\omega_i}(q)\dot{q}$$

$$K = \frac{1}{2}\dot{q}^T \sum_{i=1}^n [m_i J_{v_i}(q)^T J_{v_i}(q) + J_{\omega_i}(q)^T R_i(q) I_i R_i(q)^T J_{\omega_i}(q)] \dot{q}$$

$$K = \frac{1}{2}\dot{q}^T D(q)\dot{q}$$

# Potential Energy for N Link Robot

$$P_i = g^T r_{ci} m_i$$

$$P = \sum_{i=1}^n P_i = \sum_{i=1}^n g^T r_{ci} m_i$$

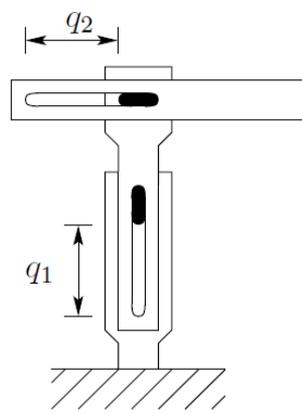
# Eular-Lagrange Equation of a Robot

$$D(q)\ddot{q} + C(q, \dot{q})\dot{q} + g(q) = \tau$$

$$\begin{aligned} c_{kj} &= \sum_{i=1}^n c_{ijk}(q)\dot{q}_i \\ &= \sum_{i=1}^n \frac{1}{2} \left\{ \frac{\partial d_{kj}}{\partial q_j} + \frac{\partial d_{ki}}{\partial q_j} - \frac{\partial d_{ij}}{\partial q_k} \right\} \dot{q}_i \end{aligned}$$

Christoffel Symbols of the first order

# Example 2D Cartesian (PP)



$$v_{c1} = J_{v_{c1}} \dot{q}$$

$$J_{v_{c1}} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1 & 0 \end{bmatrix}, \quad \dot{q} = \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

$$v_{c2} = J_{v_{c2}} \dot{q}$$

$$J_{v_{c2}} = \begin{bmatrix} 0 & 0 \\ 0 & 1 \\ 1 & 0 \end{bmatrix}$$

$$K = \frac{1}{2} \dot{q}^T \{ m_1 J_{v_c}^T J_{v_{c1}} + m_2 J_{v_{c2}}^T J_{v_{c2}} \} \dot{q}$$

$$D = \begin{bmatrix} m_1 + m_2 & 0 \\ 0 & m_2 \end{bmatrix}$$

$$P = g(m_1 + m_2)q_1$$

$$\phi_1 = \frac{\partial P}{\partial q_1} = g(m_1 + m_2), \quad \phi_2 = \frac{\partial P}{\partial q_2} = 0$$

$$\begin{aligned} (m_1 + m_2)\ddot{q}_1 + g(m_1 + m_2) &= f_1 \\ m_2\ddot{q}_2 &= f_2 \end{aligned}$$

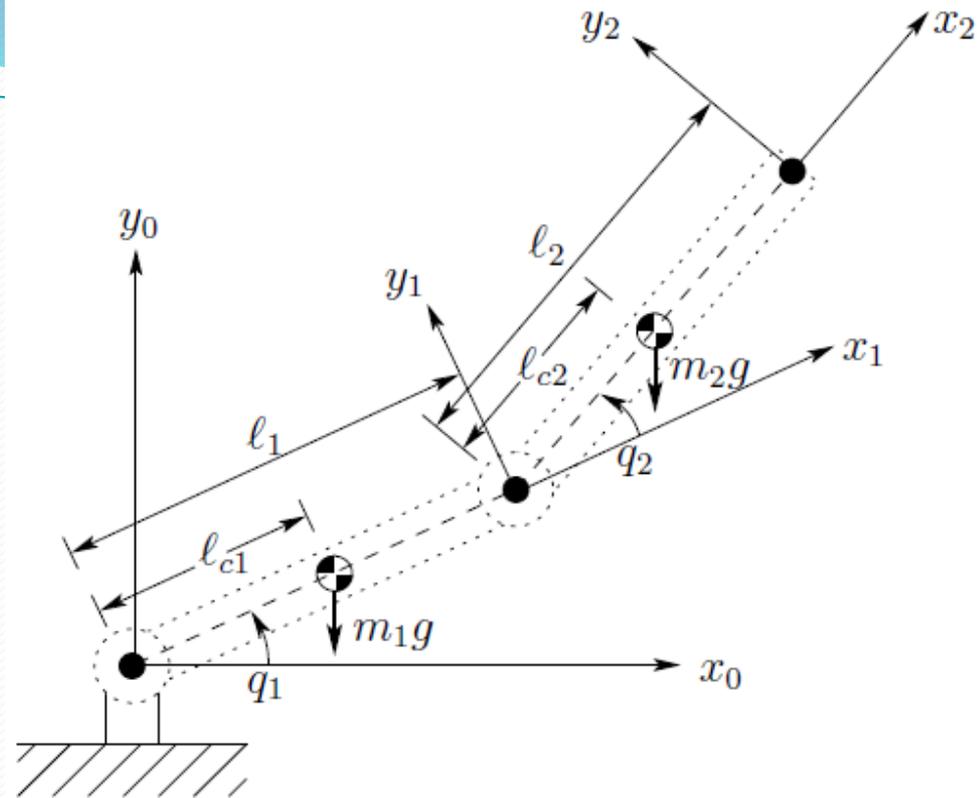
# Planar Elbow

$$v_{c1} = J_{v_{c1}} \dot{q}$$

$$J_{v_{c1}} = \begin{bmatrix} -l_c \sin q_1 & 0 \\ l_{c1} \cos q_1 & 0 \\ 0 & 0 \end{bmatrix}$$

$$v_{c2} = J_{v_{c2}} \dot{q}$$

$$J_{v_{c2}} = \begin{bmatrix} -l_1 \sin q_1 - l_{c2} \sin(q_1 + q_2) & -l_{c2} \sin(q_1 + q_2) \\ l_1 \cos q_1 + l_{c2} \cos(q_1 + q_2) & l_{c2} \cos(q_1 + q_2) \\ 0 & 0 \end{bmatrix}$$



$$\frac{1}{2} m_1 v_{c1}^T v_{c1} + \frac{1}{2} m_2 v_{c2}^T v_{c2} = \frac{1}{2} \dot{q} \{ m_1 J_{v_{c1}}^T J_{v_{c1}} + m_2 J_{v_{c2}}^T J_{v_{c2}} \} \dot{q}$$

# Planar Elbow

$$\omega_1 = \dot{q}_1 k, \quad \omega_2 = (\dot{q}_1 + \dot{q}_2) k$$

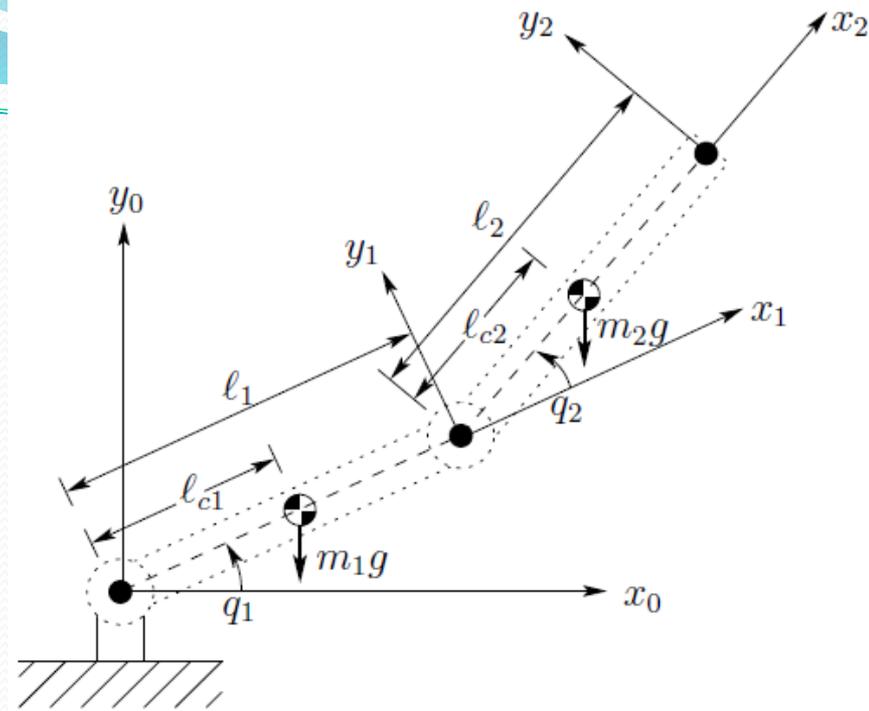
$$\frac{1}{2} \dot{q}^T \left\{ I_1 \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix} + I_2 \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix} \right\} \dot{q}$$

$$D(q) = m_1 J_{v_{c1}}^T J_{v_{c1}} + m_2 J_{v_{c2}}^T J_{v_{c2}} + \begin{bmatrix} I_1 + I_2 & I_2 \\ I_2 & I_2 \end{bmatrix}$$

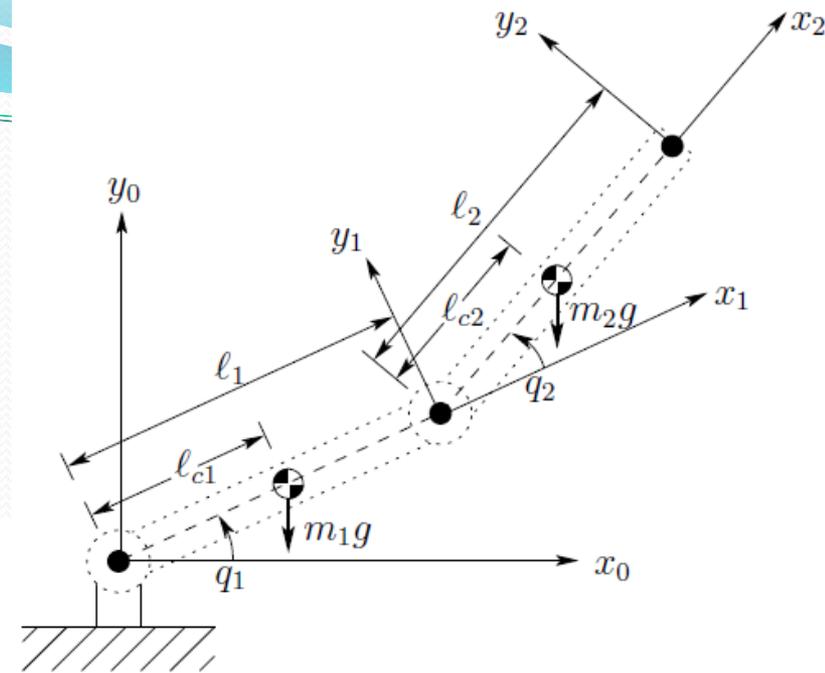
$$d_{11} = m_1 \ell_{c1}^2 + m_2 (\ell_1^2 + \ell_{c2}^2 + 2\ell_1 \ell_{c2} \cos q_2) + I_1 + I_2$$

$$d_{12} = d_{21} = m_2 (\ell_{c2}^2 + \ell_1 \ell_{c2} \cos q_2) + I_2$$

$$d_{22} = m_2 \ell_{c2}^2 + I_2$$



# Planar Elbow



$$c_{111} = \frac{1}{2} \frac{\partial d_{11}}{\partial q_1} = 0$$

$$c_{121} = c_{211} = \frac{1}{2} \frac{\partial d_{11}}{\partial q_2} = -m_2 l_1 l_{c2} \sin q_2 =: h$$

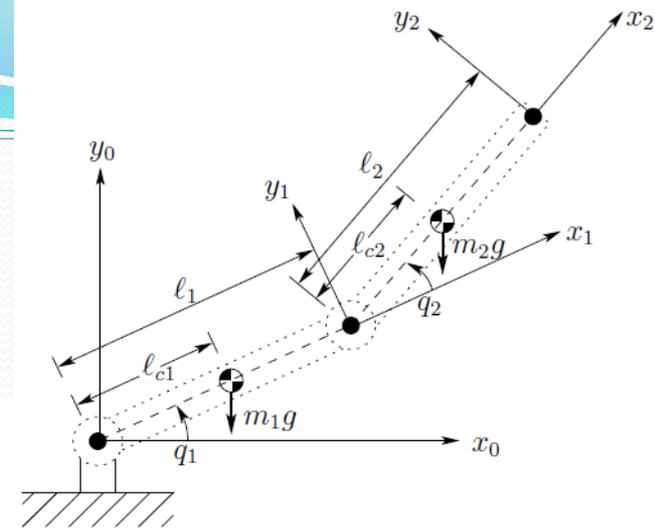
$$c_{221} = \frac{\partial d_{12}}{\partial q_2} - \frac{1}{2} \frac{\partial d_{22}}{\partial q_1} = h$$

$$c_{112} = \frac{\partial d_{21}}{\partial q_1} - \frac{1}{2} \frac{\partial d_{11}}{\partial q_2} = -h$$

$$c_{122} = c_{212} = \frac{1}{2} \frac{\partial d_{22}}{\partial q_1} = 0$$

$$c_{222} = \frac{1}{2} \frac{\partial d_{22}}{\partial q_2} = 0$$

# Planar Elbow



$$P_1 = m_1 g l_{c1} \sin q_1$$

$$P_2 = m_2 g (\ell_1 \sin q_1 + \ell_{c2} \sin(q_1 + q_2))$$

$$P = P_1 + P_2 = (m_1 \ell_{c1} + m_2 \ell_1) g \sin q_1 + m_2 \ell_{c2} g \sin(q_1 + q_2)$$

$$\phi_1 = \frac{\partial P}{\partial q_1} = (m_1 \ell_{c1} + m_2 \ell_1) g \cos q_1 + m_2 \ell_{c2} g \cos(q_1 + q_2)$$

$$\phi_2 = \frac{\partial P}{\partial q_2} = m_2 \ell_{c2} g \cos(q_1 + q_2)$$

$$d_{11}\ddot{q}_1 + d_{12}\ddot{q}_2 + c_{121}\dot{q}_1\dot{q}_2 + c_{211}\dot{q}_2\dot{q}_1 + c_{221}\dot{q}_2^2 + \phi_1 = \tau_1$$

$$d_{21}\ddot{q}_1 + d_{22}\ddot{q}_2 + c_{112}\dot{q}_1^2 + \phi_2 = \tau_2$$

$$C = \begin{bmatrix} h\dot{q}_2 & h\dot{q}_2 + h\dot{q}_1 \\ -h\dot{q}_1 & 0 \end{bmatrix}$$